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Review 1 **Cleaner production of cementitious materials containing bioag-** ² **gregates based on mussel shells: a review.** ³

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Abstract: This text proposes a bibliographic review on bioaggregates obtained from mussel shells 15 and similar materials, evaluating the main properties altered with the use of this type of recycled 16 aggregate in cementitious materials. The bibliographic analysis highlights the main problems and 17 challenges of using bioaggregates, related to the presence of organic impurities and chlorides and 18 due to the lamellar and flat shape of the grains, which impair adhesion in the transition zone. The 19 advantages of mussel shell bioaggregates include the limestone-based chemical composition, inert 20 and compatible with the application, and the specific mass close to conventional aggregates. Re- 21 garding the use in cementitious materials, in general, there is a reduction in workability, an increase 22 in incorporated air, porosity and water absorption, resulting in a reduction in compressive strength. 23 Even so, it is observed that lower replacement levels, especially in fine aggregates, make it possible 24 to use bioaggregates in cementitious materials in different applications, such as: structural concrete, 25 coating mortar and sealing systems. The positive points are related to the thermal insulation pro- 26 moted and the reduction in density, which allows for various uses for cementitious materials with 27 bioaggregates, such as: lightweight concrete, permeable concrete, and thermal and acoustic insula- 28 tion mortars. It is concluded that the use of bioaggregates in concrete and mortars is viable, but the 29 need for more experimental work to solve the main problems encountered, such as high-water ab- 30 sorption and low compressive strength, is highlighted. 31

Keywords: mortars, bioaggregates, mussel shell, sustainability. 32

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1. Introduction 34

Aggregates are construction materials used in the production of cementitious mate- 35 rials, such as concrete and mortar, in paving and earthworks or in rockfill works. Their 36 essential characteristics are the fact that they are chemically inert, adding volume to ce- 37 mentitious materials and helping to control shrinkage [1]. In this context, bioaggregates 38 emerge, natural materials extracted from plant or animal sources and used as fillers for 39 concrete and mortars. Examples include bioaggregates of plant origin, such as açaí seeds 40 [2] and palm kernels [3] and bioaggregates of animal origin, such as mussel shells and 41 other similar products, illustrated in Figure 1 [4]. The advantage of using this type of ag- 42 gregate is the high availability of the resource and the associated low added value. The 43 main disadvantages are the need for cleaning and impurity control treatments and the 44 need for a grinding step or particle size adjustment. Even with this information, it is 45

essential to highlight the need for new sources of aggregates, due to the high consumption 46 of this material in civil construction works. 47

Figure 1. Bioaggregate produced from mussel shells. 49

It is known that aggregates are obtained from the exploitation of natural resources, 50 which are quickly depleted and sometimes involve the removal of native vegetation, in 51 areas of permanent preservation, generating a variety of conflicts of interests and imply- 52 ing the most acute atmospheric impact (AWOYERA; THOMAS; KIRGIZ, 2022). The an- 53 nual global consumption of aggregates exceeds 50 billion tons every year, of which con- 54 crete production uses between 64 and 75% [6], the majority of which comes from rivers, 55 the seabed or of the restingas. In some countries, the aggregates used in the production of 56 mortars and concrete were obtained in quarries, producing other notable impacts, de- 57 stroying natural habitats, generating airborne particulates, and transforming the environ- 58 ment. Inexorably, the aggregate production process carried out in quarries involves min- 59 ing, crushing, grinding and sieving, inevitably leading to high energy consumption, earth- 60 quakes, generation of particulates and the most undesirable aggregation of $CO₂ [7]$. 61

Currently, due to the urgency of the matter, many solid wastes are being used as 62 alternative materials in the production of mortars and concrete, especially in countries 63 with high rates of greenhouse gas generation [8]. Some of the waste used in previous stud- 64 ies includes rubber to make green and clean floors and subfloors [9], construction and 65 demolition waste, such as aggregates for permeable concrete [10], incorporation of plastic 66 aggregates in high strength reinforced concrete beams [11] and use of agricultural waste 67 as pozzolanic materials and aggregates [12]. 68

In this scenario, several clear opportunities for framing new substitute materials for 69 aggregates can leverage regional development through sustainable routes, which add 70 value to waste, turning them into by-products. New investment opportunities, lower-cost 71 sustainable housing, waste reduction and job creation can be generated [13]. This is the 72 case of bioaggregates, which appear as an alternative to conventional aggregates. 73

In the case of bioaggregates of animal origin, it is common to analyze shells, the re- 74 sistant and inedible defensive shells of shellfish [6]. These materials stand out for their 75 origin in natural assembly processes which, analyzed using appropriate science, reveal 76 important lessons to be imitated in deepening the life cycle [14] and are subject to recy- 77 cling. These structures can present, on average, 97% polycrystalline CaCO³ (calcite, arag- 78 onite) and a small biological polymeric percentage of polysaccharides (chitin), proteins 79 and glycoproteins [15]; generally, they are discarded inappropriately, causing significant 80 environmental impact, generating ammonia, hydrogen sulfide and other harmful gases, 81 due to the decomposition of residual carrion, adhered to the shells, in addition to visual 82 pollution [16], generating problems of hygiene due to the lack of sanitary control, causing 83 the proliferation of insects and rodents, as they are often thrown on the streets, in back- 84 yards, beaches, slopes and mangroves, as shown in Figure 2 (D et al., 2023; MELAIS et al., 85 2023). 86

Figure 2. (a) Shells on the beach of Sidi Salem, Algeria; (b) Disposal of mussel shells on 88 Recife beach, Brazil. 89

Another relevant factor that justifies the use of bioaggregates from shells is the high 90 generation of this material. In 2020, aquatic food resources reached an all-time high of 214 91 million tons, about US\$424 billion. The production of aquatic animals was more than 60% 92 higher than the average in the 1990s, surpassing the growth of the world population, 93 thanks to aquaculture production [12]. The high production of aquatic resources is accom- 94 panied by the high generation of shells and other waste that can be used in construction 95 materials, such as bioaggregates, for example. 96

In 2022, shellfish production was around 17.7 million tonnes, making up approxi- 97 mately 23% of global aquaculture industry production [12]; These molluscs are bivalves 98 of the most common species, which represent around 89% of the entire class, including 99 mussels (sururu), oysters, pectens, scallop abalones (scallops), whelks, clams and cockles 100 (budigão) [6]. The Sururu, for example, has a bivalve shell and its body lives inside, 101 formed by two equal parts, called valves, which are joined by an organic ligament. The 102 most common genera are Perna Perna and Mytella falcata (MENEZES; MARQUES; DE 103 SOUZA, 2022), in several coastal countries such as Brazil and Spain. 104

Furthermore, it should be noted that in 2023, there are records from more than 40 105 mussel producing countries, totaling a production of more than 15 million tons of waste, 106 of which more than 4 million are discarded at sea, with the rest being distributed in land- 107 fills. and outdoors, as illustrated in Figure 2. Due to this fact, visual pollution and the 108 proliferation of microorganisms, insects and rodents are common [20]. Another relevant 109 fact is that in general 88% of the mass of sururu is made up of shells, significantly impact- 110 ing the generation of this material as waste (MENEZES; MARQUES; DE SOUZA, 2022). 111 These numbers indicate the need to develop alternative solutions, as is the case with the 112 application of bioaggregates highlighted in this research. 113

Another relevant point that justifies the analysis of bioaggregates from the use of 114 shells or other animal waste is related to the value of the oceans, which should not be 115 understood only in an economic sense, but also due to its social value. The fishing indus- 116 try employs around 200 million people in capturing, harvesting and processing fish prod- 117 ucts and provides more than 17% of animal protein worldwide [21]. It is known that, 118 mainly in coastal areas, residents and tourists consume the mollusk, being highly appre- 119 ciated as seafood and being an important source of protein. However, the high demand 120 for these foods causes the shells to be discarded incorrectly in several coastal areas, as seen 121 in Figure 2. 122

In addition to the high number of generations of this residue, another important point 123 that justifies international scientific interest is the fact that mollusc shells present re- 124 sistance properties and potential for the formation of nucleation points, improving the 125 transition zone between matrix and aggregate [13]. Therefore, studies using this type of 126 bioaggregates are becoming increasingly common. In this context, the objective of this 127 research is to carry out a bibliographical review on the use of bioaggregates of animal 128 origin in cementitious materials, proving the potential use of this material in the 129

will be evaluated. 131 132

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2. Bioaggregates obtained from mussel shells: 133

As discussed in the introduction, bioaggregates of animal origin mainly include mol- 134 lusk shells, such as mussels, or similar materials. This section will discuss the main infor- 135 mation about this type of material when applied to cementitious materials. 136

production of concrete and mortars. Mainly works using mussel shells or similar materials 130

2.1. Bibliometric analysis: 138

A bibliometric analysis was carried out using the Scopus database. The key words 139 used in the research were mussel AND shell AND mortar OR concrete OR aggregate. 140 Through this information it was possible to find 104 documents, published until 2024, as 141 indicated in Table 1. It is clear that the topic gained more prominence after 2011, when the 142 number of publications on the subject grew. However, the number of works is still very 143 low when compared to other more relevant topics, such as recycled aggregates or poz- 144 zolanic materials. It is hoped that this review will help to increase the number of works 145 on this topic. 146

Table 1. Bibliometric analysis of articles on bioaggregates of animal origin. 147

Figure 3 shows the map of correlated words. Some important information is ob- 149 served, such as: the main applications of this type of bioaggregates, in cement, concrete, 150 mortars and/or coating mortars; the main controlled properties of materials, such as: me- 151 chanical properties (compressive strength, tensile strength in flexion), thermal insulation, 152 water absorption and particle size distribution; and the main information about the mate- 153 rials used, such as the fact that mussel shells are based on calcite or calcium carbonate. 154 This information will be taken into consideration in the subsequent topics of the biblio- 155 graphic review and in the discussion of the most relevant information about bioaggregates 156 of animal origin. 157

Figure 3. Bibliometric analysis of bioaggregates of animal origin. 159

Regarding the origin of the countries of the publications highlighted in this biblio- 160 metric analysis, the following stand out mainly: Spain, with 18 publications; Malaysia 161 with 12 publications; China with 8 publications; and countries such as the United States 162 of America, Italy, France, Chile and Denmark, with 4 publications in each country. It is 163 observed that the geography of these studies is well divided, but other countries with an 164 extensive maritime region do not stand out in this scenario. It is hoped that this literature 165 review will help disseminate relevant information about studies on bioaggregates ob- 166 tained from mollusk shells or similar materials. The state of the

2.2. Physical and Chemical properties of mussel's shells: 169

Physical properties that are important in evaluating the applications of shells as bio- 170 aggregates, due to their influence on the mechanical strength and durability of concrete 171 and include specific mass (SM), maximum characteristic dimension (DCM), fineness mod- 172 ulus (FM), surface area and moisture content. Table 2 presents a summary of these prop- 173 erties, extracted from different bibliographic bases. 174

The specific mass of the bioaggregates presented in Table 2 is lower than that of con- 175 ventional aggregates or that of Ordinary Portland cement (OPC), in many studies [22,23] 176 since values for OPC vary between $3.00 - 3.10$ g/cm³. Bioaggregates, on the other hand, 177 have a more variable specific mass, in a range between 1.85 and 2.82 g/cm^3 , although there 178 is research that presents bioaggregates with values greater than 3.00 g/cm³. This highlights 179 a tendency to reduce the density of cementitious materials, promoted by mussel shells 180 and similar materials. 181

Regarding the specific surface area of bioaggregates, this factor is directly related to 182 the size of the shells and the grinding process. These factors significantly affect the size of 183 the shells. Some values found were: 1.61 μ m and 13.93 μ m, for wet and dry grinding, 184 respectively [24]; 6.27 μ m and 10.22 μ m under the same grinding conditions [25]; and av- 185 erage values of approximately $23.97 \mu m$ in the dry grinding of cockle shells, a species 186 similar to mussels [26]. These values, added to the information present in Table 2, high- 187 light the variation in the material's properties, related to heterogeneity as it is a natural 188 material. 189

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It is important to highlight that, in the case of shell ash, in general, the particles are 190 finer than ordinary Portland cement, therefore, the fineness of the mixed cement increases 191 with the level of OPC replacement. The thinner the cementitious material, the greater the 192 surface area, which consequently increases the rate of reactivity with other substances, 193 creating a binder with appreciable strength and surface area [27]. In this type of situation, 194 the material is used as a supplementary cement source. However, it should be noted that 195 the use of shells as bioaggregates requires particle size compatible with replacement, in- 196 stead of fine or coarse aggregate. 197

Bioaggregates	Especific mass	DCM		Surface area	Moisture	
	(g/cm^3)	(mm)	${\rm FM}$	(mm)	content $(\%)$	Researches
Cockle	3.03	$\overline{}$	$\overline{}$	$13.56 - 23.97$	$\overline{}$	$[27]$
Cockle	2.82	$\overline{}$	$\overline{}$	$\frac{1}{2}$	0.15	$[28]$
Cockle	2.30	4.75	2.50	$\overline{}$	0.50	[6]
Cockle	$2.50 - 2.64$	$\overline{}$	$4,40-$ 4.57	$\overline{}$	$\overline{}$	$[8]$
Mussel	3.01	$\overline{}$	$\overline{}$	29.87	$\overline{}$	$[27]$
Mussel	2.57	4.75	3.11	$\overline{}$	1.73	$[4]$
Mussel	$2.62 - 2.73$		$1.90 -$ 5.38	$\overline{}$	$\overline{}$	[8]
Mussel	2.40	5.00	\sim	$\bar{}$	3.52	$[16]$
Mussel	2.65	4.00	4.64	$\overline{}$	2.56	$[7]$
Oyster	3.09	$\overline{}$	$\overline{}$	$1.61 - 58.53$	\equiv	$[27]$
Oyster	$\overline{}$	$\overline{}$	$\overline{}$	$25.1 - 46.1$	$\overline{}$	$[25]$
Oyster	2.65				0.36	$[28]$
Oyster	$1.85 - 2.48$		$2.00 -$ 6.50			[8]
Oyster	2.42	4.75	$\overline{}$	$\overline{}$		$[29]$
Oyster	2.48	5.00	2.80	$\qquad \qquad -$	2.90	$[30]$
Oyster	2.10	4.75	2.00	$\overline{}$	$\overline{}$	$[31]$

Table 2. Physical properties of shell bioaggregates 198

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This differs from applications that propose the use of mussel shell ash as supplemen- 200 tary cementitious materials. In this context, it is more interesting to observe the DCM and 201 FM values. The values shown in Table 2 are compatible with the application of fine aggre- 202 gate, generally to coarse or medium sand. Furthermore, it is worth highlighting that the 203 moisture content values identified in Table 2 are obtained after the material washing and 204 grinding process. Before that, due to the high content of organic impurities, the associated 205 humidity is much more excessive and should be avoided. This highlights the need for 206 treatments to purify bioaggregates. 207

In the main bioaggregates used in previous studies, such as: oyster shell [32]; scallop 208 shell [33]; mussel or sururu shells [20,34]; cockle shells and mollusk shells [13]; mainly 209 compounds of naturally formed calcium carbonate (CaCO3) were found, as shown in Ta- 210 ble 3, and its mineral phases calcite and aragonite (Figure 4). The main chemical compo- 211 sition of shells is similar to that of limestone, consisting mainly of calcium oxide (CaO), 212 post-calcination, with small fractions of other oxides. The presence of calcium carbonate 213 in the form of calcite and aragonite is interesting for application as bioaggregates because 214

they are stable and chemically inert phases at room temperature. Worryingly, from a 215 chemical point of view, the presence of SO3 and SO4 appears, which can promote the 216 formation of late ettringite as a high presence in the bioaggregate. The levels found, com- 217 bined, were a maximum of 1.18% [28], a value lower than 3.00% considered problematic 218 in cement applications. Therefore, chemically the bioaggregates are compatible with the 219 proposed application. 220

According to this research, according to all types of bivalve shells, the structure of 221 mussel shells can be divided into three parts, namely, the outer layer known as periostra- 222 cum, the intermediate layer, called prismatic, and the inner nacre layer (Figure 5). A sim- 223 ilar prismatic layer rich in $CaCO₃$ was also observed in scanning electron microscopy 224 (SEM) values for oyster, cockle, sururu and scallop shells provided by [35,36], indicating 225 prismatic particles in mussel shell aggregate, contrasting with the rounded particles of 226 conventional limestone aggregate. 227

Figure 4. Diffractography of mussel shells from two species: A) C. bensoni and (B) L. marginalis. Key: $a = \text{aragonite}$; $b = \text{calcite}$. 231

Figure 5. Scheme showing the inner faces (Nacre) – rich in prismatic aragonite and calcite 234 crystals and the outer face of the mussel shell. 235

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Bioaggregates	CaCO ₃	Na ₂ O	SO ₃	MgCO ₃	SiO ₂	Al_2O_3	SO ₄	Others	Researches
Cockle	96.85	0.42	0.11	0.04	0.94	0.15	0.05	1.44	[6]
Cockle	97.13	0.37	0.13	0.02	0.98	0.17	0.07	1.13	$[28]$
Mussel	95.09	0.35	0.18	0.21	1.12	< 0.01	-	3.04	$[7] \centering% \includegraphics[width=1\textwidth]{images/TransY.pdf} \caption{The first two different values of $d=3$ and $d=4$ (left) and $d=5$ (right) and $d=6$ (right) and $d=6$ (right) and $d=6$ (right) and $d=6$ (right).} \label{fig:USY}$
Mussel	89.46	\blacksquare	0.57	\blacksquare	1.26	\blacksquare	-	0.07	$[4]$
Mussel	96.80	0.27	0.34	0.05	0.55	0.20	0.11	1.68	$[37]$
Mussel	95.60	0.44	0.34	0.03	0.73	0.13	0.11	2.62	$[28]$
Mussel	98.64	0.42	0.52	0.10	$\overline{}$		$\qquad \qquad =$	0.32	$[38]$
Oyster	95.70	0.19	0.73	0.42	1.01	0.14	0.32	1.49	$[37]$
Oyster	96.80	0.23	0.75	0.46	1.01	0.14	0.43	0.18	$[28]$
Oyster	89.56	0.98	0.72	0.65	4.04	0.42	-	3.63	$[39]$

Table 3. Chemical composition of bioaggregates from mussel shells and similar materials. 236

A shell or seashell has a hard and protective outer layer (periostracum), which is pre- 238 sent in a soft-bodied invertebrate marine animal composed of chitin-type proteins [7], and 239 can be double outer (bivalve), simple external (monovalve) or even simple internal (oc- 240 ctopus and squid). 241

Small amounts of impurities found in oyster shells were considered non-toxic when 242 incorporated into concrete [40]. It was also noted that uncalcined oyster shells indicated a 243 chloride ion content of up to 3.7%, while after calcination at 650 \degree C, a chloride ion content 244 of less than 1.34% could be achieved, depending on the duration of calcination. Based on 245 the results of leaching tests [41], it was concluded that uncrushed mussel shells can be 246 classified as inert and non-hazardous waste regulated by the European Union (EU). 247

Nacre, also known as mother-of-pearl, is one of the most fascinating animal struc- 248 tures, one of the most solid microstructures produced by molluscs (Figure 6) and its clas- 249 sical mechanical studies show that its resistance to fracture is more than a thousand times 250 greater than that of its sister. chemically precipitated inorganic, geological aragonite. As 251 if these properties were not enough, nacre has a unique combination of optical properties 252 that make it extremely attractive in jewelry and costume jewelry. This attractiveness is the 253 main reason for the development of pearl culture in the Pacific and Mexico [15]. The per- 254 iostracum, which remains unchanged throughout the animal's life, gives the shell its olive 255 green glazed exterior color. Underlying the periostracum, the mineralized layer, com- 256 posed of elongated crystals developed perpendicular to the surface of the shell, which 257 define the prismatic stratum, they are made of aragonite, one of the six polymorphs of 258 calcium carbonate, which crystallizes in the orthorhombic and represents one of the most 259 fascinating and lacking in depth in terms of origin [42]. 260

Figure 6. Section of the profile of the shell of the freshwater mussel Unio pictorum.

The presence of these crystalline forms of CaCO₃ is evident in Figure 4, where the 264 two crystalline forms are explained in the diffractogram of the sururu shell powder, com- 265 pared with geological limestone and in the thermal analysis, where the thermograms in 266 Figures 7 and 8 show the resulting from thermal degradation of powdered mussel shells. 267 In Figure 7, we can see a process that culminates at 285.5ºC, with loss of hydration and 268 interstitial water molecules, present in the shells of bivalves, as in addition to being po- 269 rous, there are components that interact with water. The most acute endothermic point, at 270 720.9°C, indicates the process of complete decomposition of the crystalline forms of 271 CaCO3, present in the shells of this mollusk, called calcination, where the loss of mass 272 occurs with the abundant formation of CO₂ [20]. 273

TG /% DTG /(%/min) 100 Peak: 837.4 °C, -0.12 lass Change: $-5.3'$ 0.0 Peak: 285.5 °C, -0.14 %/min 90 -0.5 [1.1] AMF_moldo_biovalva.ds3 -1.0 80 TG
DTG $-42.31%$ Mass Change. -1.5 70 -2.0 60 Peak: 720.9 °C. -2.55 -2.5 500 100 200 300 400 600 700 800 900 Temperature /°C

Figure 7. Thermogravimetric analysis curve for powdered mussel shells. 276

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In Figure 8, in the first thermal stage (I), between 25° C and 150° C, there is a similar 278 mass drop, relative to the humidity of the mussel shell, with a mass decay of 0.53%. In 279 stage (II), mass loss between 150°C and 500°C, between 450°C and 500°C, related to the 280 loss of organic fraction of the shell, for example polysaccharides, proteins and glycopro- 281 teins [43]. In the two cases mentioned, the mass losses are 5.31% and 3.5%, respectively, 282 in relation to the pre-calcined specimens. In stage (III), between 500° C and 800° C, also 283 present in the thermogram in Figure 7, it is possible to notice the decomposition of the 284 CaCO3 crystalline structures, originating CaO and CO2, portraying the same calcination 285 process [41]. 286

Thermal degradation analysis was also carried out under isothermal conditions in 287 the muffle furnace (2 h at 525 °C). These results determined mass losses close to 5.07 \pm 288 0.12% in organic matter, similar to all studies carried out with mussels found in the liter- 289 ature [44]. The differences between ATG (thermogravimetric analysis) and isothermal 290 degradation can be attributed to the different oven atmospheres adopted, with N2 (inert), 291 controlled and more precise monitoring of mass loss, in ATG and dynamic heating in a 292 normal atmosphere system, while in the muffle furnace, the system is open and isothermal 293 [45]. 294

Figure 8. Monitored burning process of micronized mussel shells. 296

The careful analysis of the thermographic curves presented, Figures 7 and 8, allows 298 us to affirm that there are chemical and physical peculiarities, even for shells of molluscs 299 of the same species. Furthermore, it is important that post-calcination materials present 300 calcium oxide levels comparable and compatible with geological limestone, as demon- 301 strated by diffractograms and thermographic derivatives for the two materials mentioned 302 (Figure 9), but with a more sustainable origin, given the damage caused by mining and 303 grinding of geological limestone [46]. Other considerations not made by the authors, re- 304 garding the thermographic derivative (Figure 9), are the fact that mollusk shells exceed 305 the CaCO content present in geologically explored limestone, as well as requiring lower 306 temperatures and, consequently, calcination energy, which can further favor the valoriza- 307 tion of bivalve aquaculture residue in Brazil, adding value to this productive aspect of 308 food protein. 309

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Figure 9. Comparative analysis between diffractogram and thermographic deriva- 312 tives. 313

2.3. Applications of Mussels shells: Life Cycle Analysis (LCA) 315

Recently, several studies in the area of agro-industrial waste highlight the use of tools 316 such as life cycle analysis (LCA). This is a necessary and accounting standard, developed 317 by the International Organization for Standardization (ISO), applied to the sustainable 318 development (production chain) of a given product, from cradle to grave, thinking about 319 potential environmental impacts arising from the use of energy, water and other environ- 320 mental inputs demanded, also listing the need for recycling [47]. Although LCA in the 321 agricultural sector is relatively well established, this analysis for aquaculture production 322 is not well established. When it is carried out, it refers almost exclusively to qualitative 323 aspects. The contract of the c

In view of the significant and growing quantitative aspects of aquaculture, some au- 325 thors suggest that LCA is a very important tool for evaluating the ecological compatibility 326 and impacts of seafood products [48]. After all, without reliable data it is not possible to 327 promote the application of a certain waste, without reliable data and consolidated scien- 328 tific bases [49]. 329

In search of the use and sustainability of shellfish shells (sururu) and aiming to re- 330 duce the environmental problems caused, research carried out in Brazil studied the feasi- 331 bility of incorporating powder from these shells into porcelain tile mass. The ceramic com- 332 positions were formulated from a reference industrial porcelain tile mass and sururu shell 333 powder or commercial CaCO³ varying between 0 and 7% by mass. Specimens prepared 334 by uniaxial pressing were technologically evaluated depending on the sintering tempera- 335 ture. The incorporation of up to 7%, by mass, of micronized shells, maintained the tech- 336 nological properties appropriate to the Brazilian Association of Technical Standards, 337 ABNT, for the regulation of ceramic coverings from the BI group - porcelain tiles [50]. 338

In Spain there are already initiatives aimed at valuing mussel shells from the canning 339 industry, the second largest in production in the world, with a quantity of more than 340 80,000 tons of shells per year, since 2009. There, they are managed in order to study, treat 341 and provide sustainable destination, adding value to what was previously discarded, pro- 342 moting treatment of the shells (cleaning and drying), to convert them into the majority 343 component of high purity, CaCO3, eliminating water, salt, mud and meat residues, inher- 344 ent to the shell from mussels, which previously caused effects related to the decomposi- 345 tion of organic matter and generation of leachate [22]. 346

Also in Spain, mussel shells have been applied as an additive to animal feed (source 347 of mineral salts and bulking agent), liming agent and as a constituent of fertilizers, aiming 348 to recover impoverished soils present in the country, especially in the Galicia region [15]. 349

In other European countries, however, such as Italy and France, the reality is differ- 350 ent. Italy has an estimated annual production of 6.3 tons [51]; In this case, the shells gen- 351 erated from these molluscs are discarded into the sea, certainly with unaccounted for lo- 352 gistics costs, showing a clear example of the absence of LCA [52]. 353

Another example of an LCA step is the essence of studying the adsorptive capacity 354 and the physical and/or chemical interaction between the surface of the solid adsorbent 355 and the target pollutant. This type of study is relevant and depends on the number and 356 type of adsorption sites, resulting from the intermolecular forces developed, linked to the 357 surface morphology analyzed in micronized oyster shells [53]. In this case, together with 358 cans, a source of aluminum, they proved to be effective and low cost, revealing high per- 359 formance in the adsorption of phosphates (PO4⁻³) in retention filters (Figure 10), compara- $\,$ 360 $\,$ ble to high purity ion exchange systems and high cost for treating industrial outfalls [54]. 361 362

Figure 10. Schematic model of the low-cost retention filter, with high efficiency in 364 phosphate adsorption (PO4-3). 365

Still following the treatment of sewage effluents, research identified a promising mix- 367 ture ratio of high compressive strength (0.93 MPa), as a filtering medium, using an opti- 368 mized 1:1 mixture (similar to that of Portland cement) of heavy coal ash and micronized 369 oyster shells, for phosphate fixation, in a flow of 86 cycles, with the aid of a peristaltic 370 pump [55]. With pozzolanic activity determined in this system, they believe they have 371 counteracted the adverse effects of the porosity of the proposed composite, with maxi- 372 mum PO⁴ –3 (P) fixation of 1,403 mg/g (88.4% efficiency), attributed to synergistic precipi- 373 tation effects. and adsorption. Therefore, there was effectiveness in reducing the nutrient 374 rate in coastal sediments, revealing a relevant ecological proposal in the removal of P and 375 silicates, highlighting the demand for more research, in order to optimize the filtering 376 process and investigate the increase in $NH_3(N)$ in the sediment residual $[24,56]$. 377

Recent studies have also produced valuable evidence of ACV from bivalve shells in 378 removing Cd and other toxic metals from aqueous solutions, through a chemical interac- 379 tion with calcite or aragonite, crystalline phases distinct from CaCO₃, present in shells. 380 The ability to extract Cd by the aragonite phase, calcite and micronized biogenic aragonite 381 fragments were investigated, concluding that the absorption of Cd by aragonite is fantas- 382 tically more robust than the crystalline phase [57]. 383

Through a simple heat treatment of oyster shells, another new effective adsorbent 384 was generated, as the organic matter, composed of chitin and silk protein, is removed, 385 generating greater porosity and increasing the surface area of the material, post-calcina- 386 tion; It was also found that the conversion of oyster shells into quicklime by thermochem- 387 ical treatment, not only eliminates the organic residues of oyster shells, but also produces 388 a valuable adsorbent for water and wastewater treatment, through less carbonate for- 389 mation processes. soluble, cadmium (Cd), arsenic (As), lead (Pb) or mercury (Hg) [57]. 390

Similar investigations, still related to the differences in adsorption behavior between 391 the prismatic (CP) and nacreous (CN) layers of oyster shells, common to conchiferans 392 (Figure 11), revealed different copper (Cu²⁺) removal capabilities, with interactive pre- 393 dominance of CP of 8.9 mg/g, to the detriment of CN of 2.6 mg/g, probably related to the 394 larger contact surface of CP. Furthermore, they demonstrated the high relationship be- 395 tween pH and optimal copper removal, finding that, at pH 5.5, the raw bark (CC) in 396

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powder form removed up to 99.9% of the copper, in 24 hours, in an extraction initial dose 397 of 10 mg/L [58]. 398

In South Korea, public finances increased after the establishment of a fertilizer factory 399 to recycle oyster shells and solve water eutrophication problems by transforming this ma- 400 terial into a sustainable product for efficient removal of phosphates from wastewater [55]. 401

In the United States, the zebra mussel, an invasive lake species, led to the generation 402 of large quantities of post-consumer shells, initially sent to landfills; in this case, after LCA, 403 its use as a soil conditioner, liming agent and mulch for agricultural soils has been applied 404 as an alternative [59]. 405

Peru is another country that is carrying out experiments using scallop shells to obtain 406 lime, as an input in various industrial sectors. In this country, there is research that eval- 407 uated levels of insertion of these pulverized shells into fresh and hardened concrete, con- 408 cluding that a 5% rate of cement replacement always results in an improvement in its 409 properties, whatever the w/c (water/cement) ratio. also inferred that in the grain size range 410 of 1.19 to 4.75 mm, the limit incorporation content of the shell powder of this typical mol- 411 lusk is 40%, without prejudice to the viscosity and mechanical properties of the concrete, 412 showing that perhaps the species of mollusk may influence the appropriate particle size 413 for application [33]. 414

In the Netherlands, a model of mussel tiles was created, to use shells generated in the 415 growing industry in the sector, as by-products, highlighting classic LCA results [49]. 416 Other small-scale applications of shells include controlling eutrophication in ponds and 417 water treatment systems, supplementing calcium for livestock and pets in animal feed, 418 restoring reefs, removing atmospheric pollutants, manufacturing calcium citrate, prod- 419 ucts pharmaceuticals, paper, paints and crafts, which face preliminary energy demand as 420 the main obstacle [40]. 421

There is also the possibility of reusing the shells for some shellfish aquaculture ap- 422 plications, for example, as cultivation, where it functions as a substrate on which molluscs 423 can form, grow and develop [60]. This would be a great tool in the fight against hunger in 424 several coastal countries in Latin America and Africa. In addition to all the applications 425 mentioned in this section, there is a potential for the application of mussel shells as bioag- 426 gregates in cementitious materials, which will be explored in the next topic. 427

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Figure 11. Examples of mollusk shells with micrographs of their associated calcified 430 shells on 1 μm scales, side by side. 431

2.4. Bioaggregates applied to cementitious materials: 433

In this section, the main aspects related to the use of bioaggregates in mortars and 434 concrete will be explored. It is important to make the positive and negative points of using 435 the material clear. The main negative points are related to the material's high-water ab- 436 sorption, which varies between 3 and 14%, while the saturation of natural sand is between 437 0.3 and 4.0%. This difference results in cementitious materials with workability problems, 438 requiring an increase in water and cement contents [60] which exactly contradicts the re- 439 cycling assumption. Optimal doping generally does not exceed 25% or 30%, as reported 440 in research on the topic [26,61]. This information must be taken into account in bioaggre- 441 gate studies, since a complete replacement of conventional aggregates has been rarely re- 442 ported in the literature. $\frac{443}{2}$

Another point of concern is the rheological nature of recycled aggregates (RA), being 444 another parameter that implies that maturity affects the behavior of cementitious materi- 445 als, as well as the resistance and water absorption of the evaluated material [62]. Matured 446 RA, when compared to natural aggregates (NA), reduces autogenous shrinkage in this 447 type of concrete by 20%, but can increase drying shrinkage due to the hygroscopy of the 448 material, when compared to conventional aggregates. Less rigid and earlier RA, imply 449 even more shrinkage of cementitious materials, 10 to 20% higher; that is, the use of ma- 450 tured bioaggregates, which are obtained from older mussel shells, mitigates autogenous 451 and drying shrinkage [63]. Other disadvantages will be highlighted sequentially, but they 452

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are related to an increase in total porosity and deficiencies in the paste – aggregate transi- 453 tion zone $[61]$. 454

It is worth highlighting, on the other hand, that the presence of grains of a material 455 similar to limestone present in bioaggregates is capable of reducing the width of the pores 456 present in the cement matrix, due to the chemical compatibility between matrix and ag- 457 gregate [26]. In other words, even if there is an increase in porosity, the use of aggregates 458 based on calcite and aragonite, similar to limestone, in addition to the angular shape of 459 the grains, can cause a drop in the volume of macropores, transforming them into smaller, 460 unconnected pores. in mortars with the same particle size distribution, improving the 461 workability of the material [64]. This indicates that the effect of porosity and workability 462 must always be analyzed experimentally, since bioaggregates have variable physical and 463 chemical composition. Furthermore, there may be gains in terms of reduced capillarity 464 and reduced aggressive water absorption. Another notable point is the possibility of using 465 bioaggregates in cementitious materials for thermal insulation [61]. It is observed that sev- 466 eral properties are affected by the use of bioaggregates and that the variation in the phys- 467 icochemical properties of this type of aggregate causes direct impacts on the behavior of 468 mortars and concrete. In the following topics these points will be addressed. 469

2.4.1. Influence of bioaggregate particle size 471

Particle size is an essential parameter in the study of aggregates in cementitious ma- 472 terials, defining factors such as: packaging, paste-aggregate transition zone and mechani- 473 cal resistance. In the case of bioaggregates this is no different. It is worth mentioning that 474 in most studies of mussel shells and similar materials such as aggregates for concrete and 475 mortars, it was observed that the material is used as fine aggregate [8]. This is due to sev- 476 eral factors, such as: natural size of the shells and hollow shape of the material, which 477 makes it unfeasible to be applied as coarse aggregate since the concave shape of the ma- 478 terial hinders adhesion with the matrix; high levels of water absorption, which would be 479 even more critical if the application was as coarse aggregate due to the particle size, and 480 lamellar pattern of the material, which would not be compatible with application in coarse 481 format due to regulations on the shape index [35,61]. 482

It is known that the shape index is the relationship between length and thickness of 483 the aggregate, which must be less than 3 for application in concrete. As the natural shape 484 of shell bioaggregates is lamellar, if comminution were not performed, the normative pa- 485 rameters would not be met. Illustrating this fact, some research evaluated the size of the 486 aggregate before the grinding process, obtaining a length and thickness of around 90 mm 487 and 20 mm, respectively [65]. These values indicate a shape index of 4.5, much higher than 488 the normative maximum value. Therefore, its use as fine aggregate helps to minimize this 489 problem. 490

Although it has been highlighted that most studies focus on studying bioaggregates 491 as fine aggregate, crushed shells, replacing coarse aggregate, are more suitable for the 492 production of lightweight, low-resistance concrete, due to the excessive scaling of the par- 493 ticles. of shells [44]. The primary parameter that determines the maximum level of aggre- 494 gate replacement and the granulometry that the material will be applied to is related to 495 the non-significant compromise of compressive strength and workability, properties 496 closely related to the grain size of the ground aggregate and the surface area, made avail- 497 able for them. This information must be taken into account when applying the material. 498

When studying bioaggregates replacing conventional aggregates, it is important to 499 standardize the particle size parameters, so that the study is comparative. This can be done 500 in two ways: (i) using information such as DCM and FM, compiled in Table 2 or; (ii) stand- 501 ardizing parametric granulometric curves. In the case of analysis based on DCM and FM, 502 it is recommended to use $DCM = 4.75$ mm; 2.40 mm or 1.20 mm, typical values for coarse, 503 medium and fine sand, typically used in the production of mortars and concrete [66,67]. 504 The FM must be in the range between 2.20 and 2.90 for the optimum zone or in the ranges 505

of $1.55 - 2.20$ and $2.90 - 3.50$ for the usable zones. In the case of using parametric curves, 506 a procedure is carried out as seen in Figure 12. $\frac{1}{2}$ 507

Figure 12. Particle size analysis of bioaggregates using parametric curves. 510

In the study, the authors grinded the mussel shell and separated it into two particle 512 sizes: coarse sand (particles between $0 - 4$ mm) and fine sand (particles between $0 - 1$ mm), 513 with MF of 1.90 and 4.64, respectively [7]. In the research, the authors carried out a com-
514 parison of the behavior with limestone sand, whose FM was 3.70. In this way, the authors 515 combined calculated proportions of the coarse and fine fractions of the mussel shell, ob- 516 taining sand with a parametric granulometric curve of $FM = 3.71$, compatible with the 517 conventional aggregate of the study. In this way, the analyzes carried out and the com- 518 parisons proposed by the authors are validated. Although this section aims to explore the 519 particle size of bioaggregates, it is highlighted that other parameters must be considered. 520 Some authors state that granulometry is important, but the presence of different allotropic 521 forms of CaCO3, such as calcite and aragonite, and their different reactivity and metastable 522 characteristics have more influence on mechanical properties than physical parameters 523 [46]. This will be discussed later in the text. 524

2.4.2. Influence of the specific mass of the bioaggregate. 526

The specific mass of bioaggregates is mainly affected by two factors: (i) shell size; and 527 (ii) type of material from which the shell was extracted [39]. However, when compared 528 with conventional aggregates, most bioaggregates have similar or slightly lower specific 529 masses, as seen in Table 2. Some authors highlight typical values ranging between 2.3 – 530 2.9 $g/cm³$ [8]. Natural aggregates, such as washed river sand, have a specific mass ranging 531 between $2.5 - 2.7$ g/cm³ [68]. This implies that, at least in theory, drastic changes in the 532 behavior of cementitious compounds using bioaggregates are not expected. 533

However, in practice the opposite is observed: the presence of mussel shell particles, 534 for example, impairs the workability of concrete and mortars and, in the end, there are 535 several reports that porosity increases, especially macropores. Thus, the densities of the 536 cementitious mass, both fresh and solidified, are reduced with the use of bioaggregates, 537 not due to the difference in specific mass, but rather due to an increase in porosity [15,27]. 538 Its application in coatings seems suggestive, as low-density systems tend to act as 539

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thermoacoustic comfort generators [69]. There is also no doubt that the mortar generated 540 reduces the mass load of a building, which is interesting for reducing its own weight [70]. 541 However, for structural applications, the drop in the mechanical resistance of concrete 542 and mortars generates serious limitations [44]. 543

The specific mass, together with the granulometry, also affects the packaging of the 544 final cementitious material. This can be observed through a parameter defined as packing 545 compactness. This parameter can be obtained using a single aggregate in the analysis or 546 using a combination of aggregates to check how the materials pack together. Some re- 547 search shows that the compactness of bioaggregates with mussel shells is 0.725 when used 548 with DCM = 4.75 mm, FM = 3.11 and SM = 2.57 g/cm³ [4]. Comparing the values for conventional aggregates, it is observed that for a standard room sand with $DCM = 4.75$, $SM = 550$ 2.65 g/cm³ and unspecified FM it is possible to obtain compactness of 0.76 [71], slightly 551 higher than mussel shell bioaggregate. In another research, it was observed that the use 552 of 50% bioaggregate and 50% natural aggregate results in a compactness of 0.72 [16]. Val- 553 ues above 0.70 are considered satisfactory for application to concrete and mortars. There- 554 fore, the values highlighted in this research demonstrate that mussel shell bioaggregates 555 and similar materials are compatible with this type of application. 556

2.4.3. Influence of bioaggregate morphology. The state of the state of state state of state state state state s

The greater the specific surface area of the bioaggregates, the greater the contact of 559 the material with the cement paste, improving properties such as filling and wettability, 560 enabling the system to form appreciable resistance binders [28]. $\qquad \qquad$ 561

Regarding the morphology of the material, another important point is that in mussel 562 shell particles there are many surface irregularities and microscopic holes, which is differ- 563 ent from the surface textures of other aggregates, which are relatively more uniform. This 564 demonstrates, as illustrated in Figure 13, how much the morphological aspects of bioag- 565 gregates can impact the rheological properties and the development of hydration and me- 566 chanical resistance of the cement present in concrete and mortars [46]. 567

Figure 13. Surface morphology of particles of limestone, Portland cement and mus- 570 sel shell. 571

Another important information related to the morphology of bioaggregates is linked 573 to the transition zone between paste-aggregate, known as ITZ (paste-aggregate transition 574 interface). The morphological characteristics of the mussel shell, for example, such as the 575 smooth surface of the mother-of-pearl, the presence of chitin and organic contaminants 576 and the shapes of the elongated grains, strongly damage the interfacial transition zone 577 (Figure 13), generating micro cracks, showing a poor interaction binder-aggregate and 578 again affecting the mechanical resistance of the generated composites [61]. 579

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Figure 14. ITZ (paste-aggregate transition interface) for mussel shell.

Furthermore, it is interesting to compare the ITZ of mussel shell bioaggregate with 583 other recycled aggregates, such as that obtained from construction and demolition waste 584 (RCD). In the case of the RCD, it is possible to observe the following transition interfaces: 585 ITZ1 – between the RCD and the new concrete paste/mortar produced; ITZ2 – between 586 the RCD and the old paste/mortar present in the concrete that gave rise to the recycled 587 aggregate; ITZ3 – between the old paste/mortar and the new paste/mortar of the concrete 588 produced. Therefore, the interface between RCD recycled aggregates and concrete is mul- 589 tiple and complex, weakening the material. However, it is worth highlighting that there 590 is compatibility between the transition zones, since the materials used are all cementitious. 591

In the case of mussel shell bioaggregates, ITZ4 is observed – between the shell and 592 the new concrete paste/mortar produced [72]. This information is summarized in Figure 593 15. In this context, it is worth highlighting that the advantages of using bioaggregates, 594 from the ITZ point of view, are related to a single transition zone. However, the main 595 disadvantages are related to the lack of compatibility of this zone, which adds incorpo- 596 rated air, macropores and consequently weakens the cementitious compounds. This is one 597 of the biggest challenges in using bioaggregates, which must be taken into account when 598 applying the material. 599

(a) Concrete specimen. (b) Schematic diagram. Figure 15. Comparison of the cement mass-particle transition interface of RCD and for mussel shell. 603

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2.4.4. Influence of the chemical composition of the bioaggregate. 607

The majority chemical composition of bioaggregates obtained from shells, illustrated 608 in Table 3, is based on calcium carbonate (> 90% CaCO₃), mineralologically established as 609 calcite or aragonite. It is known that the primary function of aggregates is filling, and the 610 use of reactive aggregates is not recommended. Therefore, the chemical composition of 611 bioaggregates is compatible with the proposed application, since it is very similar to the 612 composition of limestone, typically used as aggregate in concrete [73,74]. 613

Some authors have proven that micronized mussel shells are more robust sources of 614 CaCO³ than the traditionally used mineral geological sources, including enabling carbon- 615 ation points during hydration [46]. This procedure tends to reduce the pores of concrete 616 and mortar at more advanced ages, well above 28 days, as long as the shells are free of 617 organic matter in the composite and are rich in aragonite. In other words, the procedure 618 delays the setting of cement in concrete and mortars, but in the long term it reduces the 619 porosity of the material, which is favorable information for the application of bioaggregate 620 in structural concrete or coating mortar, as it reduces the percolation of chlorides. and 621 sulfates and improves durability. In other words, due to the different chemical composi- 622 tion of the lime present in the bioaggregate shells, with greater crystallinity and a more 623 reactive contact surface, it is possible for longer hydration to occur than with the use of 624 traditional aggregates. This occurs due to the formation of $Ca(OH)_{2}$ and due to the strong 625 initial assimilation of intrastructural water of the bioaggregate particles, leading to the 626 later formation of C₃S and C₂S [75]. 627

Another compound present in the chemical composition of bioaggregates is MgCO₃. 628 Some authors report levels higher than 0.50% , as seen in Table 3. It is worth highlighting 629 that the Mg^{2+} ion exerts a significant influence on the precipitation of calcium carbonate 630 and can be incorporated into the calcite crystalline network, when the Mg:Ca ratio in so- 631 lution is low or induces aragonite precipitation (metastable), when the magnesium con- 632 centration is high in the biological system that gives rise to mussel shells [76]. In other 633 words, the presence of Mg^{2+} is related to a catalysis that culminates in the precipitation of 634 a crystalline phase of monohydrate and metastable calcium carbonate (CaCO3.H2O) to- 635 gether with MgCO₃ in the form of nesquehonite [76,77]. This is problematic because both 636 $CaCO₃HeO$ and MgCO₃ require high enthalpy to dehydrate. Therefore, the procedures 637 for cleaning and drying the shells are not sufficient to rid the biogregate of these undesir- 638 able compounds, which entered the hydration process late, triggering internal tensions in 639 concrete and mortars and causing the appearance of cracks and fissures ([78]. This implies 640 that the presence of high levels of MgCO3 must be considered problematic for the appli- 641 cation of the bioaggregate. **642**

Another important point observed in Table 3 is the presence of $SO₃$ and $SO₄$. It is 643 known that the presence of sulfates in cementitious materials can be problematic as it pro- 644 motes the occurrence of late formation of ettringite. The standard recommends a maxi- 645 mum content of 3% in relation to the mass of the cement. It is observed that the levels 646 observed in Table 3 are lower values. Therefore, the presence of sulfate in bioaggregates 647 is not a critical problem, as highlighted by other authors [8]. 648

The most critical problems in the chemical composition of bioaggregates are related 649 to the presence of chlorides and organic impurities. In Table 3 it is not possible to identify 650 the presence of these components because the materials indicated in the table were ana- 651 lyzed after the shell cleaning and drying process, indicating that this treatment is suffi- 652 cient to reduce problems related to chlorides and organic impurities [33]. The presence of 653 chlorides is problematic because they can cause surface efflorescence in the concrete, re- 654 duce the pH and cause dehydration of the cement material, allowing corrosion of the re- 655 inforcement, consequently damaging the durability of the material $[79]$.). The presence of 656 organic impurities affects the setting of the cement, impairing the kinetics of the hydration 657 reactions, in addition to impairing the adhesion between the aggregate and matrix. This 658 occurs because organic impurities are present in the last layer of the shell called nacre, in 659 the form of polysaccharides (chitin), proteins and glycoprotein [80]. In other words, the 660 cleaning stage needs to be carried out appropriately so that the presence of unwanted 661 compounds is minimized, making the application of bioaggregates viable. 662

2.4.5. Workability and rheological properties of cementitious materials containing bi- 664 oaggregates. 665

In general, the behavior observed with the use of bioaggregates obtained from mus- 666 sel shells or similar materials is a reduction in the workability of cementitious materials 667 as the content of bioaggregate used increases. The reduction in workability is justified by 668 the high-water absorption of the bioaggregate, which reduces the fluidity of the material 669 and by the elongated, lamellar and flat shape of the mussel shells, increasing the dynamic 670 viscosity and internal friction of concrete and mortars, and consequently worsening the 671 fluidity parameters [8,72]. 672

Exemplifying this pattern, the reduction in the consistency of mortars with an in- 673 crease in the aggregate content present in the material stands out: 285 mm for 45% bioag- 674 gregate volume; 275 for 55% of the material; and 210 for 65% mussel shell volume [4]. In 675 general, it is observed that the main tests carried out to measure the workability of ce- 676 mentitious materials in research with bioaggregates are consistency test in mortars or 677 slump test in studies with concrete. Studies with other properties in the fresh state, such 678 as entrained air or water retention, are scarce, as are rheological tests, such as dropping 679 ball or squeeze flow. Therefore, there is a gap in these types of analysis, which are sugges- 680 tions for future work. 681

It is known that mortar, for example, is a composite basically formed by the combi- 682 nation of cement, fine aggregate and water. Additives and reinforcements can be included 683 in this system to achieve the desired physical properties of the material. When these com- 684 ponents are homogenized, a fluid or plastic system is created (cementitious hydration 685 phase), which must be easily moldable (workability). Over time, the cement forms a rigid 686 matrix that binds the rest of the components together into a durable system, similar to 687 artificial rock, with many applications. The function of the aggregate used, mainly the fine 688 one, is to reduce the demand for cement, the most expensive component, and delay dry- 689 ing, without compromising the workability of the cement mix. Furthermore, as far as pos- 690 sible, it must be able to maintain the tenacity and durability properties of the dry structure, 691 when compared to pure cement, which are only guaranteed when the concrete and mortar 692 is applied without pores or concreting niches. For this, the property of workability is fun- 693 damental [81]. 694

2.4.6 – Water absorption, porosity and capillarity of cementitious materials contain- 695 ing bioaggregates. 696

Through published research, it is observed that, in general terms, the use of mussel 697 shell bioaggregates increases the water absorption values of concrete, due to the increase 698 in porosity and reduction in the density of the material. The same pattern is observed in 699 mortars. This pattern is attributed to two factors: the shape of the bioaggregate grains, 700 which allows the formation of voids in the mortar microstructure; and the water absorp- 701 tion capacity of the shells, probably due to the existence of polymorphic variants of 702 CaCO₃, more hygroscopic such as aragonite and due to the presence of organic impurities 703 [19]. 704

The mass density of cementitious materials, both in the fresh and hardened state, also 705 presents a reduction in values, due to the high porosity that the bioaggregate promotes 706 and due to the formation of incorporated air [61]. This air forms mainly in the transition 707 zone and increases the density reduction. As a result, bioaggregates have the potential to 708 produce lightweight, low-strength concrete, due to the flaking of shell particles [48]. As 709 previously highlighted, no drastic differences are observed in the specific mass of bioag- 710 gregates and conventional aggregates. Therefore, this difference in behavior is an inter- 711 esting point to study. The study of the

Another possibility is to use mussel shell bioaggregates in the production of perme- 713 able concrete. In Algeria, studies on permeable concrete to evaluate the possibility of using 714

cockle shells, replacing crushed limestone aggregate, as a form of sustainable proposition 715 were successful. Compared to concrete with natural crushed limestone aggregates, a 20% 716 increase in porosity was observed in concrete containing cockle shells, but with the same 717 material dosage. Cockle shell aggregates had a considerable influence on the slump prop- 718 erties, reducing the density, but improving the mechanical resistance to flexural traction, 719 for the hardened state, without, however, affecting drainage, with permeability applicable 720 to the proposal for permeable concretes [18]. 721

Even though there is an increase in porosity and an increase in water absorption, an 722 interesting point highlighted in some research is that cementitious materials containing 723 bioaggregates have lower permeability to water, both pure and aggressive. Furthermore, 724 they also present lower capillarity values when compared to concrete and reference mor- 725 tars. This information indicates an increase in the durability of cementitious materials 726 with the use of bioaggregates [82]. The reasons for reduced capillarity and water perme- 727 ability are highlighted below: presence of incorporated air, which acts as a barrier to the 728 passage of water [75]; in the size of the pores, which, due to their large area, exert little 729 capillary suction force; encapsulation promoted by mussel shell grains, due to their lamel- 730 lar, rough and flat shape, which forms a barrier to the passage of aggressive water; and 731 presence of hydrophobic chitin molecules in the mussel shell bioaggregate, reducing in- 732 teractivity with water [15,44]. 733

To illustrate this information, Figure 16 presents capillarity results for mortars con- 734 taining $0 - 75\%$ replacement of natural sand with bioaggregate obtained from mussel 735 shells. The authors used two composition standards: BC, composed of mortars with a 736 lower cement content; and SC, produced with mortars richer in Portland cement. In both 737 cases, the effect of the mussel shell was the same, reducing water absorption by capillarity, 738 proving that, although there is an increase in the porosity of the material, these pores are 739 not connected and are large in size, blocking the path of water capillary, which does not 740 have enough suction to attack the mortars [15]. The mass of the mortary $\frac{741}{241}$

Capillarity uptake <> Variation percentage

2.4.7. Mechanical resistance of cementitious materials containing bioaggregates. 747

Compressive strength shows a tendency to reduce as the content of mussel shell bio- 748 aggregates in concrete and mortars increases. This effect has been reported by several au- 749 thors and is attributed to the following characteristics: (i) increase in water absorption and 750 porosity promoted by the mussel shell due to the hygroscopy of the material and due to 751

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the shape of the grains, elongated, flat and irregular, which increases the pores of the ma- 752 terial; (ii) presence of organic impurities and chlorides that impair the cement's setting 753 properties; (iii) increase in entrained air and consequently low adhesion in the transition 754 zone, impairing the transfer of efforts in the cementitious materials; and (iv) problems in 755 the production of mortars and concrete due to the lower workability of the material, con- 756 taining bioaggregates [34,38,61,75]. The contract of the contr

Although this effect is highlighted by several authors, it is important to highlight that 758 the use of mussel shells, mainly as fine aggregate, at levels of up to 25% does not cause a 759 reduction in mechanical resistance, statistically speaking, in relation to the reference com- 760 position [61]. This evidence the viability of using mussel shell bioaggregate, generating all 761 the economic and environmental advantages described previously [83]. $\frac{762}{20}$

Another important point is the need to carry out cleaning treatments on mussel shells 763 and similar materials before using them as aggregates. Figure 17 presents the results of 764 compressive strength of mortars containing 20, 30 and 40% replacement of fine aggregate 765 with three types of bioaggregates: cockle, oyster and murex. Among these three aggre- 766 gates, the one with the best mechanical parameters is the murex, due to the roughness that 767 promotes adhesion, followed by the cockle and the oyster. A tendency for resistance to 768 decrease with the use of bioaggregates is also observed. An important point to be high- 769 lighted is the difference in mechanical behavior when carrying out treatments on bioag- 770 gregates. In this research, ultrasonic cleaning was carried out to eliminate organic impu- 771 rities and adsorbed chlorides. As a result, an increase in resistance was observed from 772 approximately 50 MPa to 58 MPa, in the composition containing 10% oyster. The authors 773 prove, through experimental results, the importance of cleaning the shells [70]. The pres- 774 ence of chlorides and organic impurities slows down the setting of cement, compromising 775 the strength of concrete and mortars. However, even with this effect, no results of calo- 776 rimetry tests or definition of the setting time of mortars and concretes containing bioag- 777 gregates were found in the bibliography. This is one of the gaps found in the bibliography, 778 which shows a gap in these types of analysis, which are suggestions for future work. $\frac{779}{2}$

Figure 17. (a) Compressive strength before cleaning; (b) Compressive strength after 782 the cleaning process of different types of bioaggregates. 783

Information extracted from different authors is discussed below, related to compres- 785 sive strength parameters: Despite the lower quality concrete, in terms of compressive 786 strength (15 MPa), lower than the reference concrete, Portuguese authors report mussel 787 shell concretes with applicability at ages of 28 days of curing, not compromising the min- 788 imum required by the European standard that regulates civil construction [33]. Other au- 789 thors have demonstrated that even with lower resistance values, concretes containing 790 coarse aggregate replacement with mussel shell present the possibility of developing 791 structural concrete, lighter and at a lower cost, falling within the compressive resistance 792 class at the established 28 days. in ASTM C330. Furthermore, there were gains in durabil- 793 ity, resulting in longer-lasting works, which tend to reduce future demands for cement, 794 both for renovations and reconstruction [16]. 795

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Replacing the natural aggregate with oyster shell appears to be possible. However, it 796 negatively influences the long-term strength of concrete [40]. When crushed shell is incor- 797 porated into the concrete mix, the workability of the concrete decreases, together with the 798 flexural strength and specific mass of the concrete [48]. Despite this, this material, trans- 799 formed into sand and inserted as a partial replacement for natural aggregate (sand), in 800 cement mortar, resulted in a cementitious mass that presented acceptable mechanical 801 properties, when compared to the control group, made with conventional natural aggre- 802 σ gate [18]. 803

In an experiment carried out in Russia, the dosage of mussel shells, with an abstrac- 804 tion of 6% of binder, traditional cement, revealed more effectiveness, increasing resistance 805 properties, generating increases of up to 12% in compressive strength, up to 13% in com- 806 pression axial, 14% for flexural tensile strength and up to 12% for indirect tension. The 807 deformation under compression and axial tension decreased to 9% and 12%, respectively, 808 with an increase in the elastic modulus by 15% , relative to the reference body. This result 809 is most impressive in terms of the reduction in the cost of construction materials, com- 810 pared to traditional ones, by around 17% and in the cost of civil construction by up to 15%, 811 thanks to the reduction in the percentage of predictable defects [75]. 812

Other authors have proven that it is possible to reduce the cost of lightweight con- 813 crete by using regional snail shells and palm kernel shells (endemic palm), materials 814 lighter than granite, influencing the density of the concrete. The compressive strength of 815 the composite, as usual, decreases as substituents are added to the concrete mixtures. 816 However, the cementitious material produced from a mixture ratio of 1:1.5:3, Portland 817 cement, snail shells, vegetable biomass and granite fines, respectively, presented re- 818 sistance comparable to the control specimen, attesting to the effectiveness of the combina- 819 tion in the production of lightweight concrete at an optimal level of 5% replacement of 820 fine granite. This implies that the combination of palm kernel and periwinkle (snail) shells 821 can reduce housing and environmental costs [13]. 822

2.4.8. Thermal insulation of cementitious materials containing bioaggregates. 824

The increase in porosity promoted by the use of bioaggregates based on mussel shells 825 promotes another interesting property: thermal and acoustic insulation. Although this in- 826 formation is well accepted and disseminated among authors in the field, there are few 827 studies using mussel shells in cementitious materials for thermal insulation [8].). Figure 828 18 presents the thermal conductivity results as a function of the density of mortars con- 829 taining mussel shell bioaggregate at levels from 0 to 20% replacement. It is easy to observe 830 the correlation between the two properties and that the use of mussel shells reduces the 831 thermal conductivity of mortars, mainly attributed to porosity [38]. Therefore, an interest- 832 ing type of application of bioaggregates is for the production of concrete or thermally in- 833 sulating mortars. 834

Figure 18. Relationship between density and thermal conductivity of mortars containing mussel shell bioaggregates. 837

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3. Conclusions and Suggestions for future work: 839

The main conclusions of the work are: 840

- Bioaggregates produced from mussel shells and similar materials have potential for 841 application in concrete and mortars due to their chemical composition, predominantly 842 based on CaCO₃ in the form of calcite or aragonite, compatible with limestone aggregates 843 and chemically inert. 844

- Challenges from a chemical point of view are related to the presence of organic 845 impurities, especially in the chitin layer in the external shell, and the presence of chlorides 846 and sulfates, which can delay the setting of the cement or impair the adhesion of the ag-
847 gregate with the cement paste. Research shows that carrying out simple cleaning treat- 848 ments, such as washing in running water and drying in ovens at temperatures of 100°C 849 are sufficient to remove impurities and enable the application of the material as a bioag-850 gregate. 851

- Regarding physical properties, it is observed that bioaggregates have a specific mass 852 similar to conventional aggregates and can be used in different particle sizes, with great 853 variation in MF and DMC. However, there is a greater potential for application as fine 854 aggregate, as it is less negative in the compressive strength of cementitious materials. 855

- The morphology of bioaggregates is complex, but the presence of lamellar, irregu- 856 lar, highly porous and flat particles predominate. This particle pattern harms the transi- 857 tion zone between paste and aggregate, promoting entrained air, porosity and a drop in 858 strength. However, it is worth highlighting that the transition zone is less complex than 859 using recycled construction and demolition aggregates, for example. This is an advantage 860 when applying the material. 861

- From a properties point of view, it is observed that the use of bioaggregates in con- 862 crete and mortar has a tendency to worsen workability, increase water absorption and 863 porosity, reduce density and cause damage to mechanical properties. On the other hand, 864 there is a tendency to reduce thermal conductivity, suggesting an improvement in insula-
865 tion properties. This pattern is justified by the high-water absorption of the bioaggregate, 866 irregular, lamellar and porous particles, which impair adhesion to the cement paste, the 867 presence of organic impurities and chlorides and other factors such as an increase in the 868 viscosity of cementitious materials in the fresh state. 869

- However, several authors demonstrate that the use of lower levels of bioaggregate, 870 generally up to 25%, does not harm the mechanical properties of concrete and mortars, 871 emerging as an eco-friendly solution for disposing of mussel shell waste, for example. 872 Other possible applications are porous or permeable concrete; concrete and light mortars; 873 material for covering, sealing or laying blocks; or even as mortars for thermal and acoustic 874 insulation. In this way, viable solutions for the use of mussel shell bioaggregates in ce- 875 mentitious materials are observed. **876** and **876** and **876** and **876** and **876** and **876**

As a suggestion for future work, the following stand out: 877

- Characterization of mussel shell bioaggregates, using techniques such as: Los An- 878 geles abrasion tests, aggregate strength and tenacity tests; and/or packing compactness 879 tests. 880

- Rheological tests with concrete and mortars containing mussel shell bioaggregates 881 and similar materials, through incorporated air, water retention, rheology by dropping 882 ball or squeeze flow; and rheology analysis using viscometers. 883

- Tests that evaluate the influence of bioaggregates on the reactivity of Portland ce- 884 ment, such as calorimetry tests and definition of setting times, together with complemen- 885 tary analyzes of X-ray diffraction, scanning electron microscopy or thermal analyses, aim- 886 ing to explore the phases formed or altered during cement hydration. 887

- Additional tests on thermal, acoustic, and electrical insulation of mortars and con- 888 crete with bioaggregates, as there is potential to improve these properties with the use of 889 mussel shells. 890

- Assessment of other important mechanical parameters, such as modulus of elastic- 891 ity, tensile strength in flexion or diametrical compression to prove the impact of bioaggre- 892 gates on other relevant properties. **893**

- Analysis of the pore structure and porosity of concrete and mortars containing bio- 894 aggregates with mussel shells and similar materials, using tests such as mercury intrusion 895 porosometry or micro tomography in concrete. 896

- Non-destructive tests on concrete and mortars containing bioaggregates using scler- 897 ometry, ultrasonic pulse and electrical resistivity tests. 898

- Theoretical and experimental modeling of reinforced concrete elements with bioag- 899 gregates through the analysis of beams, pillars and slabs on a reduced scale. 900

- Economic analysis of concrete and mortar containing mussel shell bioaggregates or 901 similar materials. 902

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